# Carbon Dioxide Absorption of Barium Titanate System

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The CO<sub>2</sub> absorption capability of Ba<sub>2</sub>TiO<sub>4</sub>/BaTiO<sub>3</sub> composites was evaluated. Samples prepared from BaTiO<sub>3</sub> and BaCO<sub>3</sub> powders had chemical compositions of BaTiO<sub>3</sub>, Ba<sub>2</sub>TiO<sub>4</sub>/BaTiO<sub>3</sub>, and Ba<sub>2</sub> TiO<sub>4</sub>/BaCO<sub>3</sub>. Their CO<sub>2</sub> absorption capability was estimated using mass change. The specific surface area of the obtained samples with Ba/Ti ratio of 1, 1.33, 1.67, 2 and 2.33 was, respectively, 1.8, 2.0, 1.7, 0.5 and 1.2  $\text{m}^2 \cdot \text{g}^{-1}$ . This difference originates that the grains grew during heat treatment. Although  $BaTiO_3$  showed no  $CO_2$  absorption capability,  $Ba_2TiO_4/BaTiO_3$  and  $Ba_2TiO_4/BaTiO_4$ BaCO<sub>3</sub> composite powders did. The maximum absorption amounts were calculated from the chemical reaction during. The obtained value was about 10 times larger than that estimated from absorption test. It is regarded that the Ba<sub>2</sub>TiO<sub>4</sub> reacted incompletely with CO<sub>2</sub>, indicating that the CO<sub>2</sub> absorption capability depends on the powder properties. High CO<sub>2</sub> absorption ability is attributable to balance between high Ba<sub>2</sub>TiO<sub>4</sub> loading and specific surface area. The powders after the CO<sub>2</sub> absorption test could reproduce by heating at 1373 K.

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**Key words:** CO<sub>2</sub> absorption, Dielectric material, Recycle

## Introduction

As global warming countermeasures, many policies and technologies have been proposed for the reduction of CO<sub>2</sub> emissions. In the field of energy, wider use of fuel cells<sup>1)</sup>, solar cells<sup>2)</sup>, and wind energy<sup>3)</sup> are intended to limit atmospheric CO<sub>2</sub> levels. Nevertheless, widespread practical use of these technologies will take time. Carbon dioxide capture and storage (CCS) technologies<sup>4),5)</sup> can be used in the near future as important alternatives for CO<sub>2</sub> abatement. Especially, capturing CO<sub>2</sub> is a key technology for CCS. Methods of carbon dioxide scrubbing include adsorption, amine absorption<sup>6)</sup>, molecular sieving, and membrane filtering. Recently, chemical reaction methods using CaO<sup>7)</sup> and LiOH8) have been reported.

$$CaO + CO_2 \longrightarrow CaCO_3$$
 (1)  

$$2LiOH + CO_2 \longrightarrow Li_2CO_3 + H_2O$$
 (2)

$$2L_1OH + CO_2 \longrightarrow L_{12}CO_3 + H_2O \tag{2}$$

Saito et al. reported that Ba<sub>2</sub>TiO<sub>4</sub><sup>9),10)</sup> is also available for this technique. For these materials, which have higher reaction velocity, the absorption and desorption temperatures were determined using the following thermodynamic relation.

$$Ba_2TiO_4 + CO_2 \stackrel{873 \text{ K}}{\rightleftharpoons} BaCO_3 + BaTiO_3$$
 (3)

From the viewpoint of barium element recycling,

Ba<sub>2</sub>TiO<sub>4</sub> is an interesting material because large amounts of BaTiO<sub>3</sub> used in electronic applications generates a considerable amount of waste. Consequently, the chemical reaction and thermodynamics of this material as a chemical substance are widely discussed. However, its properties as the material are scarcely reported, leaving a dearth of knowledge of its specific surface area (SSA) and particle size. Such knowledge can support the practical use of CCS using a barium titanate system.

Pfaff reported that the SSA-controlled Ba<sub>2</sub>TiO<sub>4</sub> was obtained by heating of Ba<sub>2</sub>TiO<sub>2</sub>(OH)<sub>3</sub>(OOH) at appropriate temperature<sup>11)</sup>. This method is useful to merely synthesis of Ba<sub>2</sub>TiO<sub>4</sub>. However, another reason to use Ba<sub>2</sub>TiO<sub>4</sub> as the CO<sub>2</sub> absorbent is recycling of BaTiO3 as above. Therefore, it is desirable to prepare the Ba<sub>2</sub>TiO<sub>4</sub> from BaTiO<sub>3</sub> as a starting material. It is reported that controlling chemical composition is one of the easiest way to change the SSA. For instance, the SSA of NiO-Al<sub>2</sub>O<sub>3</sub> solid solution depended on the NiO loadings<sup>12)</sup>. The powder of stoichiometry chemical composition (NiAl<sub>2</sub>O<sub>4</sub>) showed the lowest SSA. Moreover, the metal ions is well known to control the decrease in SSA at high temperature 13),14).

These results suggest that the SSA of the Ba<sub>2</sub>TiO<sub>4</sub> may be controlled by changing the Ba loading. In contrast, the change the Ba loading can lose the CO<sub>2</sub> absorption ability. Based upon the foregoing, it is thought that balance of SSA and Ba loading of the absorbent is important.

For this study, Ba<sub>2</sub>TiO<sub>4</sub>/BaTiO<sub>3</sub> composites were prepared from BaTiO<sub>3</sub> and BaCO<sub>3</sub>. Then the relation between SSA and chemical composition of the obtained samples was estimated, along with its CO<sub>2</sub> absorption capability.

### 2 Experimental procedure

High-purity BaCO<sub>3</sub> (Wako Pure Chemical Inds. Ltd., Osaka, Japan) was mixed with BaTiO<sub>3</sub> (BT-01: Sakai Chemical Industry Co., Ltd., Osaka, Japan). The Ba/Ti ratios were 1, 1.33, 1.67, 2, and 2.33. The mixtures were heated at 1373 K for 1 h (heating and cooling rate: 10 K/min). Then CO<sub>2</sub> absorption tests were conducted at 873 K (heating and cooling rate: 10 K/min) for 30 min under a 90%  $N_2$ -10%  $CO_2$  atmosphere (0.3 L/min). After absorption tests, the 2.00 g samples were heated at 1373 K for 1 h for CO<sub>2</sub> desorption tests under air atmosphere. The temperawere tures determined using thermodynamic calculation9),10). Phases formed in the powder were identified using X-ray diffractometry (XRD) with Cu Kα radiation (LabX XRD-6100; Shimadzu Corp., Kyoto, Japan). The powder sample SSA was measured using BET method with nitrogen (Gemini V: Shimadzu Corp., Kyoto, Japan).

#### 3 Results and Discussion

Fig. 1 portrays the XRD patterns of the obtained powders after heating at 1373 K. The sample with a Ba/Ti ratio of 1 consists solely of BaTiO<sub>3</sub> phase. The BaTiO<sub>3</sub> peaks decreased concomitantly with increase of the Ba/Ti ratio. At the Ba/Ti ratio of 2.33, Ba<sub>2</sub>TiO<sub>4</sub>

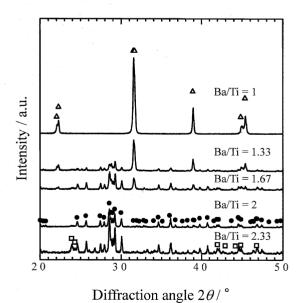


Fig. 1 XRD patterns of samples after heating at 1100 °C for 1 h.

 $\bullet$ : Ba<sub>2</sub>TiO<sub>4</sub>,  $\triangle$ : BaTiO<sub>3</sub>,  $\square$ : BaCO<sub>3</sub>

and  $BaCO_3$  were observed because the decomposition temperature of  $BaCO_3$  is about 1723 K. No chart shows any other phase.

The SSAs of the present samples are presented in Table 1. Those of the samples with Ba/Ti ratios of 1. 1.33, and 1.67 were  $1.7-2.0 \text{ m}^2 \cdot \text{g}^{-1}$ . Those of samples with a Ba/Ti ratio of 2 were about  $0.5 \text{ m}^2 \cdot \text{g}^{-1}$ , which is about one-third of those listed above. All values were lower than the SSA of the raw BaTiO<sub>3</sub> powder  $(12.5 \text{ m}^2 \cdot \text{g}^{-1})$ . It is considered that the grains grew during heat treatment. The heat treatment of the mixtures was used for the chemical reaction from the mixtures to the objective materials. However, grain growth also occurred. Kwon et al. reported that the particle size changes as a function of heating temperature<sup>15)</sup>. The average size of particles used in their research was about 140 nm. Grain growth was observed at temperatures higher than 1173 K. The average particle size of the sample after heating at 1373 K was about 810 nm. For spherical particles, the relation between the particle size and SSA is described as the relation shown below.

$$d = \frac{6}{\rho \cdot A} \tag{4}$$

Therein, d,  $\rho$ , and A respectively represent the particle size, particle density, and SSA. The respective particle sizes of BaTiO<sub>3</sub> samples (Ba/Ti ratio of 1) before and after heating estimated from this equation are ca. 80 and 555 nm. These show fair agreement with Kwon's report<sup>15)</sup>. Slight differences originate from the fact that the particles are not perfectly spherical. Large decrease of the SSA of Ba<sub>2</sub>TiO<sub>4</sub> samples (Ba/Ti ratio of 2) was observed. Results show that Ba<sub>2</sub>TiO<sub>4</sub> has high sinterability. Samples with a Ba/Ti ratio of 1.33 and 1.67 have slightly higher SSA. It is inferred that they have two phases, each of which impedes their grain growth. Moreover, samples including more contents of Ba<sub>2</sub>TiO<sub>4</sub>, of which grains grow easily, showed low SSA. At the Ba/Ti ratio of 2.33, BaCO<sub>3</sub> apparently restrains Ba<sub>2</sub>TiO<sub>4</sub> particle growth.

The CO<sub>2</sub> absorption capability of the obtained samples was evaluated. The phase change of Ba<sub>2</sub>TiO<sub>4</sub> after CO<sub>2</sub> absorption and desorption testing is presented in Fig. 2. The BaCO<sub>3</sub> phase was assigned in samples after the CO<sub>2</sub> absorption test. However, the sample consists mainly of Ba<sub>2</sub>TiO<sub>4</sub>, which suggests that Ba<sub>2</sub>TiO<sub>4</sub> was not completely reacted with CO<sub>2</sub>. After desorption tests, the BaCO<sub>3</sub> reacted with BaTiO<sub>3</sub> and

Table 1 The specific surface area of the obtained samples.

						Raw material (BaTiO <sub>3</sub> )
Specific surface area/ $m^2 \cdot g^{-1}$	1.8	2.0	1.7	0.5	1.2	12.5

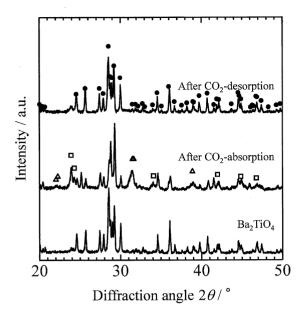


Fig. 2 XRD pattern of the samples with Ba/Ti=2 after absorption and desorption tests.

 $\bullet$ : Ba<sub>2</sub>TiO<sub>4</sub>,  $\triangle$ : BaTiO<sub>3</sub>,  $\square$ : BaCO<sub>3</sub>

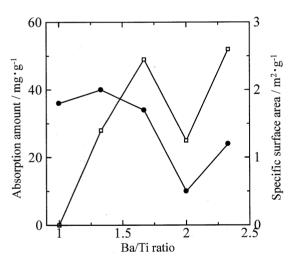


Fig. 3  $CO_2$  absorption amount and SSA as a function of  $Ba_2TiO_4$  loading in the samples.

 $\bullet$ : SSA,  $\square$ : CO<sub>2</sub> absorption

the  $Ba_2TiO_4$  was synthesized again. The  $CO_2$  absorption amount is shown in Fig. 3. The SSAs of the samples were also illustrated in Fig. 3.  $BaTiO_3$  has only slight absorption capability. Samples with a Ba/Ti ratio of greater than 1.33 showed  $CO_2$  absorption (about  $28 \text{ mg} \cdot \text{g}^{-1}$ ).

The absorption amount of the sample with Ba/Ti of 1.67 was about  $49 \text{ mg} \cdot \text{g}^{-1}$ . It is considered that this increase originates to increase of Ba<sub>2</sub>TiO<sub>4</sub>. However, the absorption amount of pure Ba<sub>2</sub>TiO<sub>4</sub> was lower than that of the samples with Ba/Ti of 1.33 and 1.67 (about  $25 \text{ mg} \cdot \text{g}^{-1}$ ). The chemical reaction of CO<sub>2</sub> absorption, described by eq. (3), can be used to calculate the maximum obtainable amounts from this

chemical reaction. The value of  $114~\rm mg\cdot g^{-1}$  was obtained, which is much higher than the measured value. For the  $Ba_2TiO_4$  phase, which is regarded as indispensable for  $CO_2$  absorption, the chemical reaction occurs only at the particle surface. In contrast, the sample with Ba/Ti ratio of 2.33 showed the highest  $CO_2$  absorption. This samples includes  $BaCO_3$  other than  $Ba_2TiO_4$ . However, the SSA of the sample is more than twice as high as that of the pure  $Ba_2TiO_4$ .

These results suggested that both SSA and chemical composition are important for  $CO_2$  absorbance. Moreover, it indicates that SSA of absorbance should increase at the cost of amount of  $Ba_2TiO_4$  phase in some cases.

## 4 Summary

The  $Ba_2TiO_4/BaTiO_3$  and  $Ba_2TiO_4/BaCO_3$  composites powders were prepared by solid-state reaction of  $BaTiO_3$  and  $BaCO_3$  powders. Their  $CO_2$  absorption capability was estimated. We conclude that  $Ba_2TiO_4$  loading and SSA affected the barium titanate system's  $CO_2$  absorption capability. To improve  $CO_2$  absorption, the Ba/Ti ratio should be set as greater than 2, and particles should be small.

The following results were obtained:

- 1) The crystalline phase of the powder with a Ba/Ti ratio of 1 was BaTiO<sub>3</sub> phase. It showed no CO<sub>2</sub> absorption capability.
- 2) The  $Ba_2TiO_4/BaTiO_3$  composite powders (Ba/Ti ratio of 1.33 and 1.67) have  $CO_2$  absorption capability. The  $CO_2$  absorption amount increased with increasing the  $Ba_2TiO_4$  loading. However, the  $Ba_2TiO_4$  reacted incompletely with  $CO_2$ .
- 3) The sample with a Ba/Ti ratio of 2 consists solely of Ba<sub>2</sub>TiO<sub>4</sub> phase with SSA of  $0.5 \, \text{m}^2 \cdot \text{g}^{-1}$ . It showed lower CO<sub>2</sub> absorption capability than the above composites. It is considered that the low CO<sub>2</sub> absorption capability originates to the low specific surface area of the sample.
- 4) The  $Ba_2TiO_4/BaCO_3$  composite powder (Ba/Ti ratio of 2.33) also has  $CO_2$  absorption capability. It is regard that it has higher specific surface area than  $Ba_2TiO_4$ .

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## チタン酸バリウム系材料による二酸化炭素の吸収

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 $Ba_2TiO_4/BaTiO_3$  複合材の  $CO_2$  吸収能を評価した。 $BaTiO_3$  と  $BaCO_3$  粉末から作製したサンプルの化学組成は  $BaTiO_3$ ,  $Ba_2TiO_4/BaTiO_3$  と  $Ba_2TiO_4/BaCO_3$  であった。これらの  $CO_2$  吸収能は,重量変化で求めた。Ba/Ti 比が 1, 1.33, 1.67, 2, 2.33 のサンプルの比表面積は,それぞれ,1.8, 2.0, 1.7, 0.5, 1.2  $m^2 \cdot g^{-1}$  であった。この違いは熱処理中の粒成長によるものである。 $BaTiO_3$  は  $CO_2$  吸収能を示さなかったが, $Ba_2TiO_4/BaTiO_3$  と  $Ba_2TiO_4/BaCO_3$  複合材は  $CO_2$  吸収能を示した。化学反応式から最大  $CO_2$  吸収量を計算したところ,実験で得られた値の約 10 倍だった。これのため  $Ba_2TiO_4$  が  $CO_2$  と完全には反応しておらず, $CO_2$  吸収能が単に化学反応だけでなく,粉末の特性に依存したと考えられる。また,高い  $CO_2$  吸収能は  $Ba_2TiO_4$  量と高比表面積のバランスによると示唆された。また, $CO_2$  吸収した後の複合材は, $CO_2$  吸収能は  $CO_2$  吸収能であることで再生することができた。